

Speed Reducers for Precision Motion Control

Harmonic Drive® Reducer Catalog

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- Differential Gear FD
- Engineering Data

NOTE: This is a section from our full Reducer Product Catalog. Page numbers are for reference only.



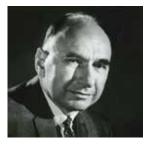
Excellent Technology for Evolving Industries

Harmonic Drive® actuators utilize high-precision, zero-backlash Harmonic Drive® precision gears and play critical roles in robotics, semiconductor manufacturing equipment, factory automation equipment, medical diagnostics and surgical robotics. Additionally, our products are frequently used in mission-critical spaceflight applications which capture the human spirit.

With over 50 years of experience, our expert engineering and production teams continually develop enabling technologies for the evolving motion control market. We are proud of our outstanding engineering capabilities and successful history of providing customer specific solutions to meet their application requirements.

Harmonic Drive LLC continues to develop enabling technologies for the evolving motion control market, which drives the pace of global innovation.





C. Walton Musser Patented Strain Wave Gearing in 1955

Operating Principle of Harmonic Drive® Gears

A simple three-element construction combined with the unique operating principle puts extremely high reduction ratio capabilities into a very compact and lightweight package. The high-performance attributes of this gearing technology including, zero-backlash, high-torque-to-weight ratio, compact size, and excellent positional accuracy, are a direct result of the unique operating principles.



Wave Generator

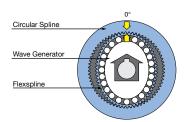
The Wave Generator is a thin, raced-ball bearing fitted onto an elliptical hub. This serves as a high-efficiency torque converter and is generally mounted onto the input or motor shaft.

Flexspline

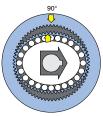
The Flexspline is a non-rigid, thin cylindrical cup with external teeth on the open end of the cup. The Flexspline fits over the Wave Generator and takes on its elliptical shape. The Flexspline is generally used as the output of the gear.

Circular Spline

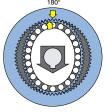
The Circular Spline is a rigid ring with internal teeth. It engages the teeth of the Flexspline across the major axis of the Wave Generator ellipse. The Circular Spline has two more teeth than the Flexspline and is generally mounted onto a housing.



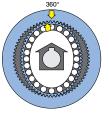
The Flexspline is slightly smaller in diameter than the Circular Spline and usually has two fewer teeth than the Circular Spline. The elliptical shape of the Wave Generator causes the teeth of the Flexspline to engage the Circular Spline at two opposite regions across the major axis of the ellipse.



As the Wave Generator rotates the teeth of the Flexspline engage with the Circular Spline at the major axis.



For every 180 degree clockwise movement of the Wave Generator, the Flexspline rotates counterclockwise by one tooth in relation to the Circular Spline.



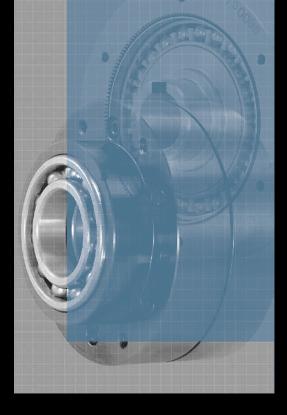
Each complete clockwise rotation of the Wave Generator results in the Flexspline moving counterclockwise by two teeth from its original position, relative to the Circular Spline. Normally, this motion is taken out as output.

■ Development of HarmonicDrive® Speed Reducers



Harmonic Drive® gears have been evolving since the strain wave gear was first patented in 1955. Our innovative development and engineering teams have led us to significant advances in our gear technology. In 1988, Harmonic Drive successfully designed and manufactured a new tooth profile, the "S" tooth. Since implementing the "S" tooth profile, improvement in life, strength and torsional stiffness have been realized. In the 1990s, we focused engineering efforts on designing gears featuring space savings, higher speed, higher load capacity and higher reliability. Then in the 2000s, significant reduction in size and thickness were achieved, all while maintaining high precision specifications.





FD Series

Differential Gear FD

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NOTE: This is a section from our full Reducer Product Catalog. Page numbers are for reference only.

Features =



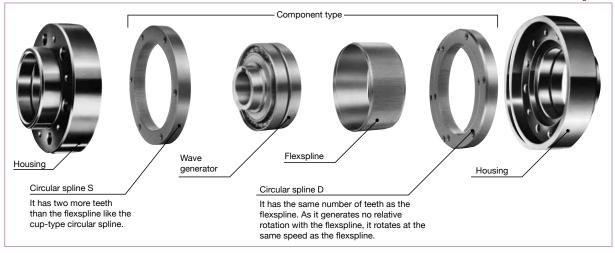
Differential gear FD series

The FD series is an extremely compact differential unit that allows you to fine-tune the phase and timing during operation. Like the pancake component sets, the FD series consist of four parts. FD is available as a gear unit with housing or as a component set without a housing. The housing enables additional gears or pulleys to be directly mounted onto it.

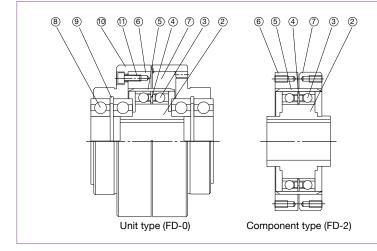
Features of FD series

- Pancake component set
- Ultra compact differential unit
- Backlash is very small and unit requires no assembly adjustment
- Very large reduction ratios between the adjusting shaft and the output, it allows precision position adjustment and requires little torque for adjusting the shaft
- Easily installed into OEM equipment
- Component set consists of only four parts and is mounted coaxially

Structure of the FD series Fig. 288-1





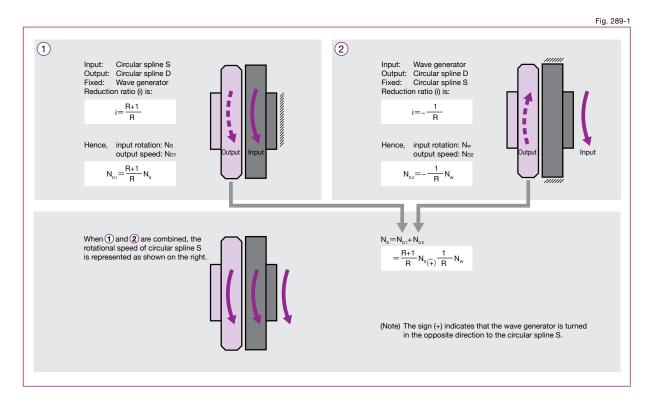


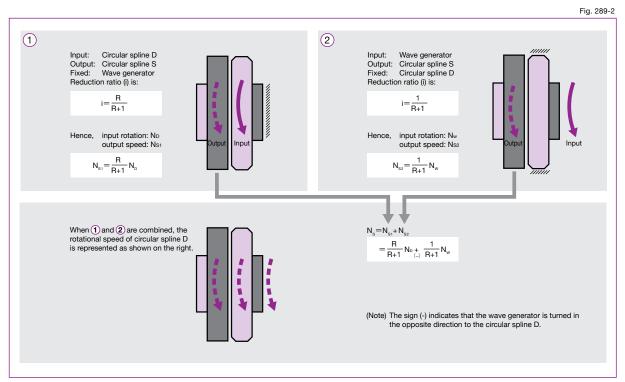
Part No.	Part name
1	Wave generator
②2	Wave generator plug
③₃	Wave generator bearing
4 ,	Retainer presser
6	Flexspline
6	Circular spline S
0	Circular spline D
8	Ball bearing
9	Internal C-type stop ring
0	Housing
11	Bolt with hexagonal hole

(Note) How to tell circular spline D from circular spline S The peripheral chamfering of circular spline D is larger than that of circular spline S.

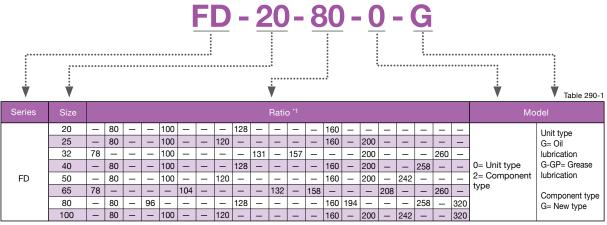
Rotational direction and reduction ratio

The rotational direction is the same as the FB series (Page 105). This section describes how to use the unit as a differential unit. (R indicates the reduction ratio value in the ratings table.)





Ordering Code =

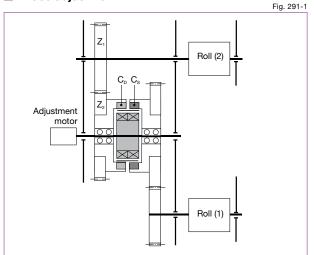


The reduction ratio value is based on the following configuration: Input: wave generator, fixed: circular spline S, output: circular spline D

How To Use

Usage example

■ Phase adjustment



Brake a unit to adjust the phase of two rolls, normally an adjusting motor, and rotate it in the system: roll (1) \rightarrow Cs \rightarrow CD \rightarrow Roll (2). When the phase of Roll (2) against Roll (1) needs to be adjusted, the adjusting motor should be rotated. Stop the motor after adjustment and return Roll (2) to the original rotation.

(Calculation formula)

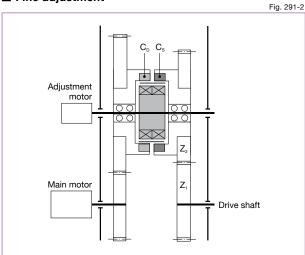
When the adjusting motor is fixed, the rotational speed of Roll (2) should be No. Assuming that the adjusting motor rotates in Nw, rotational speed N of the roll is expressed as follows.

Formula 291-1

$$N = N_0 \pm \frac{1}{R} \left(\frac{Z_2}{Z_1}\right) N_w$$

The sign is minus (-) when the wave generator rotates in the same direction as the circular spline. It is plus (+) when the wave generator rotates in the opposite direction.

■ Fine adjustment



This is the method to fine-tune the speed and timing of the drive shaft by the adjusting motor without changing the rotational speed of the main motor.

(Calculation formula)

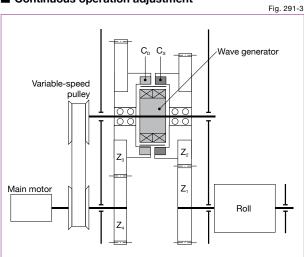
When the adjusting motor is fixed, the rotational speed of the drive shaft is expressed as follows.

Formula 291-2

$$N=N_0 \pm \frac{1}{R+1} \left(\frac{Z_2}{Z_1}\right) N_w$$

The sign is plus (+) when the wave generator rotates in the same direction as the circular spline. It is minus (-) when the wave generator rotates in the opposite direction.

■ Continuous operation adjustment



This is a unit to continuously make a slight change to the rotational speed of the roll. The rotation of the main motor has the following two routes.

- (1) $Z_4 \rightarrow Z_3(C_0) \rightarrow Z_2(C_S) \rightarrow Z_1 \rightarrow Roll$
- (2) Variable-speed pulley → wave generator → C_S (Z₂) → Z₁ → Roll

The speed change of the roll is given by (2).

(Calculation formula)

Assuming that the rotation of the variable-speed pulley is zero, the rotational speed of the roll rotated by the main motor is No. When the rotation of the wave generator, namely the variable-speed pulley, changes from N1 to N2, rotational speed N of the roll is expressed as follows.

$$N=N_0 \pm \frac{1}{R+1} \left(\frac{Z_2}{7}\right) \left(N_1 \text{ to } N_2\right)$$

The sign is plus (+) when the wave generator rotates in the same direction as the circular spline. It is minus (-) when the wave generator rotates in the opposite direction.

Engineering Data

Differential Gear FD

Example of assembly

■ Paper-cutting machine

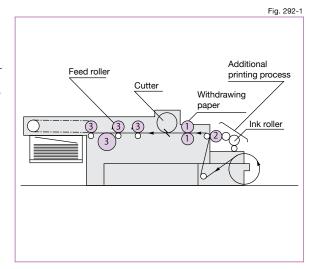
The right-hand figure shows an example of a general application that is used for the mechanism shown below.

Outline of operation

Rollers (1), (2) and (3) are interlocked based on the rotation of the cutter. Roller (2) feeds paper for further printing on the printed paper that is then extracted by Roller (1). Roller (2) adjusts the misaligned printing.

Roller (1) adjusts the printed paper so that it will be cut in the correct position by Roller (2). Roller (3) makes further adjustment following Roller (1).

You can change the phase between the rollers by building a Harmonic differential gear in Units (1), (2) and (3) without stopping the unit



■ Printer (film material)

The following process is essential for printing on elastic material.

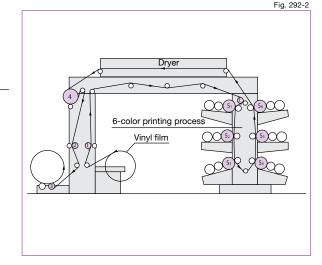
- 1. A device to adjust printing misalignment by expansion and contraction
- 2. A device to continue tensioning film to prevent wrinkling

Outline of operation

The film material is withdrawn by (a).

6 tensions film between 6 and 6 to prevent wrinkling.
② tensions film betwenn 6 and 2 to prevent slackening in the printing process 5. In the printing process 5, all rollers from 6 to 6 are used for 6-color printing. Adjustment is made to 5 based on 6, to 6 based on 6, and so on up to 6 by the Harmonic differential gear.

The harmonic differential is built in for all rollers from (1a) to (5a).



Difference between the differential gear and the Harmonic differential gear

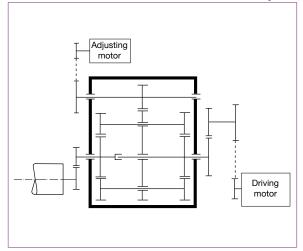
Table 293-1

Differential gear	Harmonic differential gear
As many gears are required in the differential device, the device increases in size, causing problems in design, and is difficult build it in.	As the Harmonic differential gear includes the differential mechanism, it can be designed to be of compact size and is easily built in.
A unit using a plant gear causes a lot of backlash and is disadvantageous in position and timing precision.	As it causes very small backlash, it is advantageous in position and timing precision.
It is not easy to fine tune compared to the Harmonic differential gear.	As it has a large reduction ratio, it can produce very fine tuning.
Noisy gear sound	Very quiet.

That shown in the right-hand figure is a differential gear used in a printer maker. It is an example of very smart, compact design using the Harmonic differential gear.

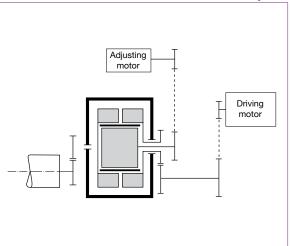


Fig. 293-1



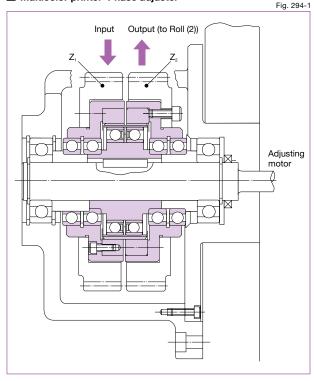
Using the Harmonic differential gear

Fig. 293-2



Example of design

Multicolor printer Phase adjuster



The figure is an example of a Harmonic differential gear unit (FD-0) built in as a phase adjuster for the roll of a multicolor

The adjusting motor is fixed during normal operation, and the rotation at Z₁ is transmitted to Z₂ almost at a ratio of 1:1. To adjust the phase of only Roll (2), rotate the adjusting motor to generate a small rotational difference. After adjustment, stop the motor to bring Roll (2) back to the original rotational speed.

Gear selection data

The selection data of the number of teeth, Z1, Z2, Z3 and Z4, of the gear is shown when rotational speed N_1 is equal to N_2 , namely $i = \frac{N_2}{N_1} = 1$.

$$\frac{N_2}{N_1} = i = \frac{Z_1}{Z_2} \cdot \frac{Z_D}{Z_S} \cdot \frac{Z_3}{Z_4} \dots (i)$$

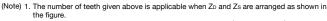
Zs: the number of teeth of circular spline S ZD: the number of teeth of circular spline D

Here
$$i_{\scriptscriptstyle D} = \ \frac{Z_{\scriptscriptstyle D}}{Z_{\scriptscriptstyle S}} \ \ \left(\text{or} \ \frac{R}{R+1} \right)$$
 makes

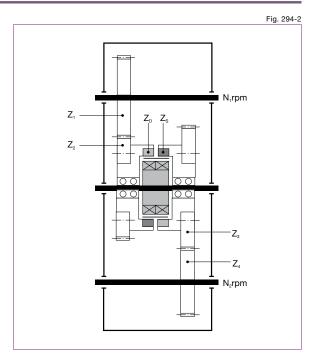
$$i = \frac{Z_1}{\overline{Z}_2} \cdot \frac{Z_3}{\overline{Z}_4} \cdot i_D$$

Tabl 294-1

i _D		<u>Z</u> , · <u>Z</u> , · <u>Z</u> ,										
80 81	18 .18 16 20	18 .27 16 30	15.27 16.25	18.27 20.24	21.27 20.28	27 .39 26 .40						
120 121	22 ·22 20 ·24											
128 129	15.43 16 40	33 .4 <u>3</u> 32 40	43.63 42 64									
160 161	14.2 <u>3</u> 16 20	21 .2 <u>3</u> 20 24	23.77 22 80	23.35 25 32								



- 2. The difference in the number of teeth is adjusted to $Z_1 Z_2 \le 3$ and $Z_3 Z_4 \le 3$.
- 3. It is useful to break down in to prime numbers to use a different number of teeth It is not possible to break down in to prime numbers for R=79, 96, 100, 131, 208 and 258.



Calculation example

This is to calculate the torque required for the number of teeth of the gear, rotational speed, adjustment quantity and adjustment based on the example shown in the right-hand figure (Fig. 267-1).

[Usage condition]

In Figure 267-1

Speed around the roller V= 60m/min

Length around the roller $L_w = 500$ mm

Roller torque $T_w = 7kg-m$

Rotational speed of the drive shaft N₁=500rpm

Rotational speed of the roller $N_4 = \frac{V}{L_w} = \frac{60}{0.5} = 120 rpm$

Under these conditions, select model number 25 of differential gear with reduction ratio R=80, review whether or not this mode I number is appropriate, as well as the number of teeth and adjustment torque.

■ The number of teeth of each gear (selection of Z₁, Z₂, Z₃ and Z₄)

The total reduction ratio is as follows.

$$\frac{Z_{2}}{Z_{1}} \times \frac{Z_{4}}{Z_{3}} = \frac{2^{3} \times 3 \times 5}{2^{2} \times 5^{3}} \times \frac{2^{4} \times 5}{3^{4}} = \frac{2^{5}}{3^{3} \times 5} = \frac{2^{3}}{3 \times 5} \times \frac{2^{2}}{3^{2}} = \frac{8}{15} \times \frac{4}{9} = \frac{16}{30} \times \frac{16}{36} \times \frac$$

Hence

$$Z_1 = 30$$
, $Z_2 = 16$, $Z_3 = 36$, $Z_4 = 16$

■ Calculation of rotational speed

The rotational speed of each gear is shown below.

$$Z_4$$
: $N_1 = 500 \text{rpm}$

$$Z_3$$
: $N_3 = \frac{Z_4}{Z_3}$ • $N_1 = \frac{16}{36} \times 500 = 222.2 \text{rpm}$

$$Z_2$$
: $N_2 = \frac{C_s}{C_D} \cdot N_3 = \frac{81}{80} \times 222.2 = 225 \text{rpm}$

 Z_1 : N_4 =120rpm

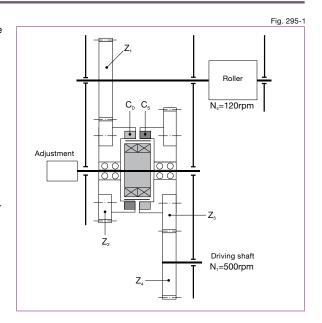
■ Adjustment quantity

The misalignment (adjustment quantity), $\triangle\theta$, at the roller is expressed as follows when the adjusting wave generator rotates once (360°).

$$\triangle \theta = \frac{Z_2}{Z_1} \cdot \frac{1}{R} \cdot \theta = \frac{16}{30} \times \frac{1}{80} \times 360^{\circ} = 2.4^{\circ}$$

Therefore, the adjustment quantity is expressed as follows in the circle.

$$\triangle \theta = \frac{2.4^{\circ}}{360^{\circ}} \times 500 \text{mm} = 3.3 \text{mm}$$



■ Adjustment torque required

The torque required for adjustment is expressed as follows.

$$T = T_w \cdot \frac{Z_z}{Z_1} \cdot \frac{1}{R} \cdot \frac{1}{\eta} = 7kg-m \times \frac{16}{30} \times \frac{1}{80} \times \frac{1}{0.6}$$

= 0.07kg-m

(η: efficiency)

Technical Data

Rating table

The rated torque at each rotational speed is shown below.

Table 296-1

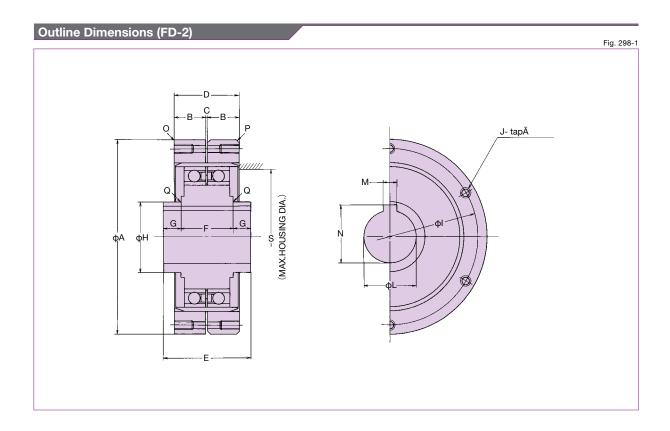
																				Tabl	le 296-
Rotational s rpm	peed	35	00	28	50	17	50	14	50	11:	50	96	60	87		75	60	60	0	50	0
Size	Ratio	Nm	kgfm	Nm	kgfm	Nm	kgfm	Nm	kgfm	Nm	kgfm	Nm	kgfm	Nm	kgfm	Nm	kgfm	Nm	kgfm	Nm	kgfm
	80	29	3.0	30	3.1	30	3.1	30	3.1	30	3.1	30	3.1	30	3.1	30	3.1	30	3.1	30	3.1
	100	30	3.1	31	3.2	36	3.7	36	3.7	36	3.7	36	3.7	36	3.7	36	3.7	36	3.7	36	3.7
20	128	31	3.2	34	3.5	42	4.3	43	4.4	43	4.4	43	4.4	43	4.4	43	4.4	43	4.4	43	4.4
	160	32	3.3	35	3.6	42	4.3	45	4.6	48	4.9	49	5.0	49	5.0	49	5.0	49	5.0	49	5.0
	80	46	4.7	50	5.1	57	5.8	57	5.8	57	5.8	57	5.8	57	5.8	57	5.8	57	5.8	57	5.8
	100	49	5.0	53	5.4	67	6.8	67	6.8	79	8.1	79	8.1	79	8.1	79	8.1	79	8.1	79	8.1
	120	52	5.3	55	5.6	70	7.1	70	7.1	80	8.2	82	8.4	89	9.1	91	9.3	96	9.8	96	9.8
25	160	54	5.5	57	5.8	71	7.2	73	7.4	80	8.2	83	8.5	89	9.1	92	9.4	98	10	108	11
	200	55	5.6	59	6.0	71	7.2	74	7.5	80	8.2	84	8.6	89	9.1	92	9.4	98	10	108	11
	78	98	10	108	11	108	11	108	11	108	11	108	11	108	11	108	11	108	11	108	11
	100	108	11	118	12	137	14	147	15	157	16	157	16	157	16	157	16	157	16	157	16
	131	108	11	118	12	137	14	157	16	167	17	176	18	176	18	196	20	206	21	206	21
32	157	108	11	118	12	137	14	157	16	167	17	176	18	176	18	196	20	206	21	216	22
-	200	108	11	118	12	137	14	157	16	167	17	176	18	176	18	196	20	206	21	216	22
	260	108	11	118	12	137	14	157	16	167	17	176	18	176	18	196	20	206	21	216	22
	80	196	20	196	20	196	20	196	20	196	20	196	20	196	20	196	20	196	20	196	20
	100	235	24	245	25	265	27	265	27	265	27	265	27	265	27	265	27	265	27	265	27
	128	235	24	245	25	294	30	314	32	343	35	363	37	372	38	372	38	372	38	372	38
40	160	235	24	245	25	294	30	314	32	343	35	363	37	372	38	392	40	421	43	451	46
10	200	235	24	245	25	294	30	314	32	343	35	363	37	372	38	392	40	421	43	451	46
	258	235	24	245	25	294	30	314	32	343	35	363	37	372	38	392	40	421	43	451	46
	80	353	36	353	36	353	36	353	36	353	36	353	36	353	36	353	36	353	36	353	36
	100	441	45	470	48	549	56	559	57	559	57	559	57	559	57	559	57	559	57	559	57
	120	441	45	470	48	549	56	588	60	637	65	666	68	666	68	666	68	666	68	666	68
50	160	441	45	470	48	549	56	588	60	637	65	676	69	696	71	745	76	794	81	843	86
	200	441	45	470	48	549	56	588	60	637	65	676	69	696	71	745	76	794	81	843	86
	242	441	45	470	48	549	56	588	60	637	65	676	69	696	71	745	76	794	81	843	86
	78		_	_	_	764	78	764	78	764	78	764	78	764	78	764	78	764	78	764	78
	104	_	_	_	_	1030	105	1100	112	1180	120	1190	121	1190	121	1190	121	1190	121	1190	121
	132	_	_	_	_	1030	105	1100	112	1180	120	1250	128	1290	132	1380	141	1460	149	1570	160
65	158	_	_	_	_	1030	105	1100	112	1180	120	1250	128	1290	132	1380	141	1460	149	1570	160
	208	_	_	_	_	1030	105	1100	112	1180	120	1250	128	1290	132	1380	141	1460	149	1570	160
	260	_	_	_	_	1030	105	1100	112	1180	120	1250	128	1290	132	1380	141	1460	149	1570	160
	80	_	_	_	_	1370	140	1370	140	1370	140	1370	140	1370	140	1370	140	1370	140	1370	140
	96	<u> </u>	_	_	_	1800	184	1800	184	1800	184	1800	184	1800	184	1800	184	1800	184	1800	184
	128	_	_	_	_	2040	208	2180	222	2340	239	2490	254	2570	262	2710	277	2710	277	2710	277
	160	_	_	_	_	2040	208	2180	222	2340	239	2490	254	2570	262	2740	280	2950	301	3130	319
80	194				_	2040	208	2180	222	2340	239	2490	254	2570	262	2740	280	2950	301	3130	319
	258					2040	208	2180	222	2340	239	2490	254	2570	262	2740	280	2950	301	3130	319
	320	 			_	2040	208	2180	222	2340	239	2490	254	2570	262	2740	280	2950	301	3130	319
	80		_	_	_	2470	252	2470	252	2470	252	2470	252	2470	252	2470	252	2470	252	2470	252
	100		_	_	_	3720	380	3720	380	3720	380	3720	380	3720	380	3720	380	3720	380	3720	380
	120				_	3720	382	3980	406	4280	437	4560	465	4710	481	4740	484	4740	484	4740	484
	160					3720	382	3980	406	4280	437	4560	465	4710	481	5010	511	5390	550	5720	584
100	200				_	3720	382	3980	406	4280	437	4560	465	4710	481	5010	511	5390	550	5720	584
	242			_	_	3720	382	3980	406	4280	437	4560	465	4710	481	5010	511	5390	550	5720	584
	320		_	_	_	3720	382	3980	406	4280	437	4560	465	4710	481	5010	511	5390	550	5720	584
	1 020					3120	302	0000	+00	1200	101	1000	+00	77 10	701	3010	011	10000	1000	3720	307

(Note) 1. Rotational speed: This indicates the rotational speed of the wave generator if used as a reducer.

This indicates the relative rotational speed of the wave generator and the circular spline if used as a differential unit.

- 2. The torque against a rotational speed of 2,500 rpm or less is equal to the torque for 500 rpm.
- 3. The allowable momentary torque allows up to 200% of the torque at a rotational speed of 1,450 rpm.

Dimensions (FD-0)								Table 297-1 Unit: mm
Size	20	25	32	40	50		80	100
ΦА	85	95	120	145	185	235	290	360
фВь7	52	65	85	100	125	140	180	210
фС	20	30	40	50	60	70	90	110
D	73	81	95	113	132	147	178	212
E	1	1	1	1	1	1	1	1
F	44	45	55	65	80	117	129	155
G	12.5	16	18	20	22	12	21.5	25.5
Н	2	2	2	4	4	3	3	3
I	38	40	50	68	78	87	106	130
J	17.5	20.5	22.5	22.5	27	30	36	41
φК	70	80	105	125	155	195	240	290
L	6	6	6	6	6	6	8	8
М	M4×7	M5×8	M6×9	M8×11	M10×13.5	M12×23	M12×23	M14×27
фNн7	12	20	30	35	40	50	65	80
O _{Js9}	4	6	8	10	12	14	18	22
Р	13.8	22.8	33.3	38.3	43.3	53.8	69.4	85.4
Q	#6004	#6006	#6008	#6010	#6012	#6014	#6018	#6022
Mass (kg)	2.0	2.6	5.0	8.3	17	34	59	118



Dimensions (FD-2)								Table 298-1 Unit: mm
Size Symbol	20	25	32	40	50	65	80	100
фА ₉₇	70	85	110	135	170	215	265	330
В	12	14	18	21	26	35	41	50
С	1	1	1	1	1	1	1	1
D	25	29	37	43	53	71	83	101
E	38	40	50	68	78	87	106	130
F	21.5	25	30	44	54	59	74	92
G	8.25	7.5	10	12	12	14	16	19
фНл6	20	30	40	50	60	70	90	110
фІ	60	75	100	120	150	195	240	290
J	6	6	6	6	6	6	8	8
K	M3×6	M4×8	M5×10	M6×12	M8×16	M10×20	M10×20	M12×24
фLн7	12	20	30	35	40	50	65	80
M _{Js9}	4	6	8	10	12	14	18	22
N	13.8	22.8	33.3	38.3	43.3	53.8	69	85.4
Oc	0.2	0.2	0.2	0.4	0.4	0.4	0.4	0.4
Pc	1	1.5	1.5	1.5	1.5	1.5	2	2
QR	0.5	1	1	1	2	1	1.5	2
S	42	53	69	84	105	138	169	211
Mass (kg)	0.6	1.0	2.0	3.6	7.2	14	26	48

Efficiency

The efficiency of the differential gear unit (FD-0) varies depending on the power transmission route.

(1) The efficiency when the power enters from circular spline $\ensuremath{\mathsf{S}}$ (or D) to transmit the rotation to circular spline D (or S)

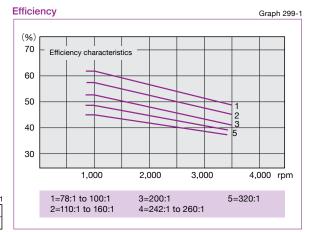
For oil lubrication: About 90Ā For grease lubrication: About $80\bar{A}$

(2) The efficiency for obtaining the input torque required by the wave generator for phase adjustment and to use it as a reducer is shown in Graph 299-1.

Table 200-1

Load torque	Rated torque in rating table
Lubrication	Oil lubrication (approx. 40°C)

(Note) The efficiency decreases by about 10for grĀĀease lubrication.



Moment of inertia

The value of GD² of each part is shown in Table 299-2.

Table 299-2 Unit: (X10-4kgm2)

								mit. (XTO Rgin
Size				40		65	80	100
Wave generator (except the outer race of the wave generator)	1.44	3.63	12.9	37.0	112	366	1020	3050
Circular spline S, D Outer ring of the wave generator	13.7	33.8	125	326	1020	3440	9270	27000
	15.2	37.5	138	363	1140	3810	10300	30100
IV Support bearing (4)	2.91	8.98	23.4	451	104	205	646	1590
V Casing (right and left casing total)	52.6	69.0	204	484	1660	6220	15700	43200

Max. allowable rotational speed

The maximum allowable rotational speed means:

- 1. The rotational speed of the wave generator when used as a reducer
- 2. The relative rotational speed of the wave generator and the circular spline when used as a differential unit

(1) For oil lubrication

Table 299-3

Unit: rpm

Size	20	25	32	40	50	65	80	100
Max. allow. rotational speed	6000	5000	4500	4000	3500	3000	2500	2000

(2) For grease lubrication

Table 299-4 Unit: rpm

								- · · · · · · · · · · · · · · · · · · ·
Size	20	25	32	40	50	65	80	100
Max. allow. rotational speed	3600	3600	3600	3300	3000	2200	2000	1700

Lost motion and spring constant

See age 120 for a definition of lost motion and the spring constant. \bar{A} Hysteresis loss and the spring constant of the differential gear is the value when either the wave generator or the circular spline is fixed and a torque is applied to the other circular spline.

Table 300-1

0:	Lost motic	n (arc min)	Spring constant (kgm/min)				
Size	± load (kgm)	Standard product (max.)	Load (kgm)	Spring constant			
20	0.12	40	3.69	0.9			
25	0.23	37	7.20	2.1			
32	0.46	35	15.78	4.4			
40	0.92	33	29.50	7.8			
50	1.73	29	57.60	16			
65	3.9	27	126.7	27			
80	7.4	26	236.2	52			
100	14.4	24	460.8	100			

Design Guide

Precaution on handling

The casing and the roller bearing in using a component type (FD-2) as a differential unit should be pursuant to the unit type (FD-0).

Precautions on assembly

The FD gear may generate vibration and abnormal sound due to problems during assembly. erform assembly based on the F $\bar{A}\bar{A}$ series precautions (age 109, Fig. 109-2).Ā

Lubrication

There are two types of lubrication oil lubrication and græase lubrication. Although oil lubrication is common, grease lubrication is applicable to intermittent operation.

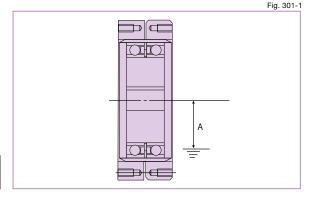
Oil lubrication

1. Type of lubricant

See age 018 for lubrication details. \bar{A}

2. Oil quantity

The oil level shall be the position shown in Table 301-1.



Oil position

Oil position Table 30										
Size	20	25	32	40	50	65	80	100		
Α	12	15	31	38	44	62	75	94		

■ Grease lubrication

Different from oil lubrication, as a cooling effect is not expected from grease lubrication, it is only available for short operation.

- Operating condition: EDĀĀ· 10or less, continuous operation for 10 minutes or ĀĀ less, the maximum allowable input rotational speed in Table 271-4 or less
- Recommended grease: ····· Harmonic Grease S-1A Ā

Note) If you use the product over EDor the maximum permissible rĀĀotational speed, the grease will deteriorate, will not work as a lubricating mechanism and will result in damaging the reducer earlier. Extreme care should be taken. $lease\ consider\ the\ unit\ type\ since\ unit\ type\ (FD-0)\ also\ comes\ in\ gr\bar{A}ease\ sealed\ type\ (NION\ OU\ L\bar{A}\bar{A}\bar{A}\bar{A}TD.\ M\ No.\ 2).\bar{A}$

Engineering Data

Engineering Data		
Tooth profile	• S tooth profile ·····	009
Rotational direction	• Cup style ·····	010
and reduction ratio	Silk hat style	010
	ancake style	011
Rating table definition	ns	012
Life		012
Torque limits		013
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Lubrication	Grease lubricant ·····	016
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	Harmonic Grease® 4 No.2Ā Oil lubricant	
	Lubricant for special	018
	environments	019
Torsional stiffness		020
Positional accuracy		021
Vibration		021
Starting torque		022
Backdriving torque		022
No-load running torqu	ue	023
Efficiency		023
Design	Design guideline	024
guidelines	• earing support of the input Ā and output shafts	025
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Assembly	• Sealing	028
guidelines	Assembly r\(\text{Aecautions}\)	028
	• edoidalstateĀĀĀĀ	029
Checking output	Checking procedure	030
bearing	How to calculate the maximum	030
	moment load	030
	average load ·····	031
	• How to calculate the radial load coefficien (X) and axial load coefficient ()Ā · · · · · · · · ·	^t 031
	How to calculate life	032
	How to calculate the life under oscillating movement	032
	How to calculate the static safety coefficient	030

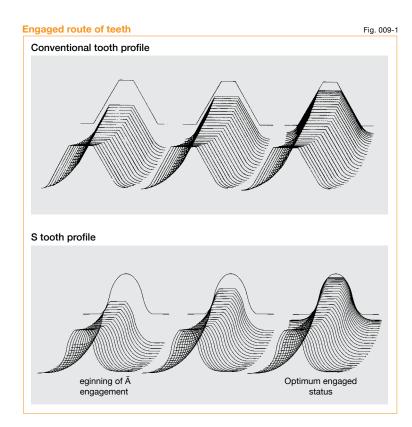
Tooth Profile

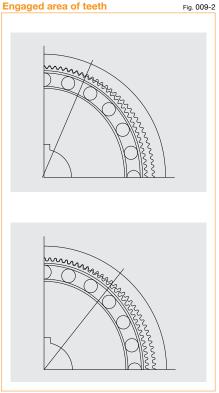
■ S tooth profile

Harmonic Drive developed a unique gear tooth profile that optimizes the tooth engagement. It has a special curved surface unique to the S tooth profile that allows continuous contact with the tooth profile. It also alleviates the concentration of stress by widening the width of the tooth groove against the tooth thickness and enlarging the radius on the bottom. This tooth profile (the tooth enables up $\bar{A}\bar{A}\bar{A}$ to 30of the total number of teeth to be engaged simultaneously $\bar{A}\bar{A}$

Additionally the large tooth root radius increases the tooth strength compared with an involute tooth. This technological innovation results in high torque, high torsional stiffness, long life and smooth rotation.

*Patented





Rotational direction and reduction ratio

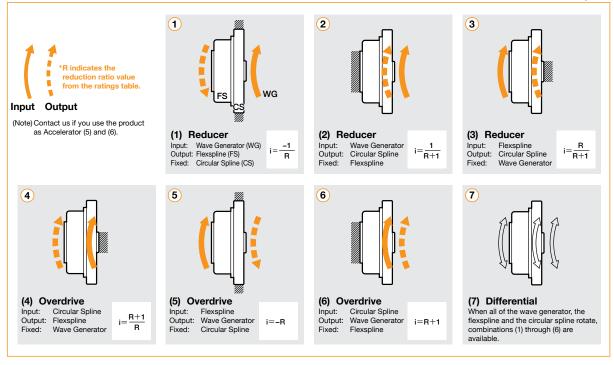
Cup Style

Series: CSG, CSF, CSD, CSF-mini

Rotational direction

Fig. 010-1

Fig. 010-2



Silk hat

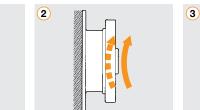
Input Output

Series: SHG, SHF, SHD

■ Rotational direction

*R indicates the from the ratings. table

(Note) Contact us if you use the product as an overdrive of (5) or (6).





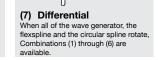
Circular Spline

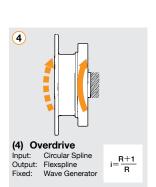
Flexspline

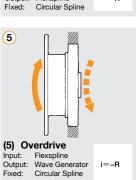
i=R+1

(3) Reducer Input: Flexspline
Output: Circular Spline Wave Generator





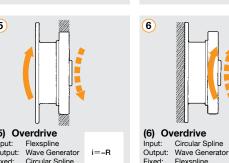




1

(1) Reducer

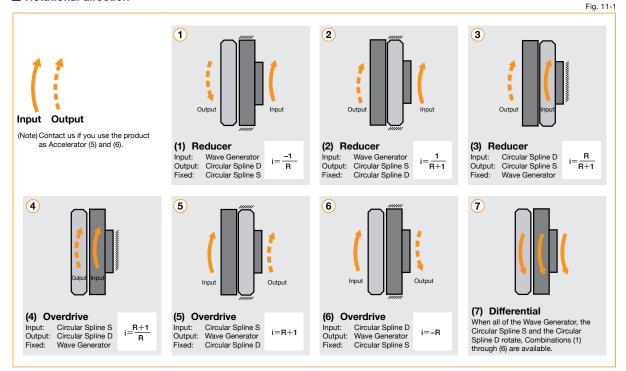
Input: Wave Generator Output: Flexspline



Pancake

Series: FB and FR

■ Rotational direction



■ Reduction ratio

The reduction ratio is determined by the number of teeth of the Flexspline and the Circular Spline

Number of teeth of the Flexspline: Zf Number of teeth of the Circular Spline: Zc

 $\begin{array}{c|cccc} & \text{Input:} & \text{Wave Generator} \\ & \text{Output:} & \text{Flexspline} \\ & \text{Fixed:} & \text{Circular Spline} \end{array} \end{array} \right\} \begin{array}{c} \text{Reduction} \\ \text{ratio} & \text{i}_1 = \frac{1}{R_1} = \frac{\text{Zf-Zc}}{\text{Zf}} \end{array}$

 $\begin{array}{c|c} \hline \text{Input:} & \text{Wave Generator} \\ \text{Output:} & \text{Circular Spline} \\ \text{Fixed:} & \text{Flexspline} \end{array} \end{array} \right\} \begin{array}{c} \text{Reduction} \\ \text{ratio} \end{array} i_2 = \frac{1}{R_2} \ = \ \frac{\text{Zc-Zf}}{\text{Zc}}$

■ R₁ indicates the reduction ratio value from the ratings table.

Example

Number of teeth of the Flexspline: 200 Number of teeth of the Circular Spline: 202

 $\begin{array}{ll} \mbox{Input:} & \mbox{Wave Generator} \\ \mbox{Output:} & \mbox{Flexspline} \\ \mbox{Fixed:} & \mbox{Circular Spline} \end{array} \right\} \begin{array}{ll} \mbox{Reduction} \\ \mbox{ratio} \end{array} i_1 = \frac{1}{R_1} = \frac{200\text{-}202}{200} = \frac{-1}{100} \\ \end{array}$

Rating Table Definitions

See the corresponding pages of each series for values.

■ Rated torque

Rated torque indicates allowable continuous load torque at rated input speed.

■ Limit for Repeated Peak Torque (see Graph 12-1)

During acceleration and deceleration the Harmonic Drive® gear experiences a peak torque as a result of the moment of inertia of the output load. The table indicates the limit for repeated peak torque.

■ Limit for Average Torque

In cases where load torque and input speed vary, it is necessary to calculate an average value of load torque. The table indicates the limit for average torque. The average torque calculated must not exceed this limit. (calculation formula: Page 14)

■ Limit for Momentary Peak Torque (see Graph 12-1)

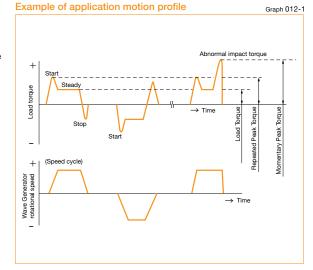
The gear may be subjected to momentary peak torques in the event of a collision or emergency stop. The magnitude and frequency of occurrence of such peak torques must be kept to a minimum and they should, under no circumstance, occur during normal operating cycle. The allowable number of occurrences of the momentary peak torque may be calculated by using formula 13-1

■ Maximum Average Input Speed Maximum Input Speed

Do not exceed the allowable rating. (calculation formula of the average input speed: Page 14).

■ Moment of Inertia

The rating indicates the moment of inertia reflected to the gear input.



Life

■ Life of the wave generator

The life of a gear is determined by the life of the wave generator bearing. The life may be calculated by using the input speed and the output load torque.

Table 012-						
	Life					
Series name	CSF, CSD, SHF, SHD, CSF-mini	CSG, SHG				
L ₁₀	7,000 hours	10,000 hours				
L ₅₀ (average life)	35,000 hours	50,000 hours				

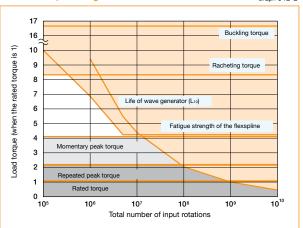
* Life is based on the input speed and output load torque from the rating table.

Calculation formula for Rated Lifetime Formula 012-1 $Lh = Ln \cdot \left(\frac{Tr}{Tav}\right)^3 \cdot \left(\frac{Nr}{Nav}\right)$ Table 012-2

		Table 012-2
	Ln	Life of L ₁₀ or L ₅₀
	Tr	Rated torque
		Rated input speed
	Tav	Average load torque on the output side (calculation formula: Page 14)
- [Nav	Average input eneed (calculation formula: Page 1/I)

Relative torque rating

Graph 012-2



- * Lubricant life not taken into consideration in the graph described above.
- * Use the graph above as reference values

Torque Limits

■ Strength of flexspline

The Flexspline is subjected to repeated deflections, and its strength determines the torque capacity of the Harmonic Drive® gear. The values given for Rated Torque at Rated Speed and for the allowable Repeated Peak Torque are based on an infinite fatigue life for the Flexspline.

The torque that occurs during a collision must be below the momentary peak torque (impact torque). The maximum number of occurrences is given by the equation below.

Allowable limit of the bending cycles of the flexspline during rotation of the wave generator while the impact torque is applied: 1.0 x 104 (cycles)

The torque that occurs during a collision must be below the momentary peak torque (impact torque). The maximum number of occurrences is given by the equation below.

Calculation formula

Formula 013-1

$$N = \frac{1.0 \times 10^4}{2 \times \frac{n}{60} \times t}$$

Allowable occurances	N occurances				
Time that impact torque is applied	t sec				
Rotational speed of the wave generator	n rpm				
The flexspline bends two times per one revolution of the wave generator.					



If the number of occurances is exceeded, the Flexspline may experience a fatigue failure.

■ Buckling torque

When a highly excessive torque (16 to 17 times rated torque) is applied to the output with the input stationary, the flexspline may experience plastic deformation. This is defined as buckling torque.

^{*} See the corresponding pages of each series for buckling torque values.



When the flexspline buckles, early failure of the HarmonicDrive® gear will occur.

■ Ratcheting torque

When excessive torque (8 to 9 times rated torque) is applied while the gear is in motion, the teeth between the Circular Spline and Flexspline may not engage properly.

This phenomenon is called ratcheting and the torque at which this occurs is called ratcheting torque. Ratcheting may cause the Flexspline to become non-concentric with the Circular Spline. Operating in this condition may result in shortened life and a Flexspline fatigue failure.

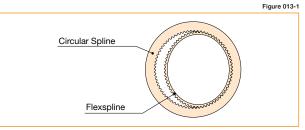
- * See the corresponding pages of each series for ratcheting torque values.
 * Ratcheting torque is affected by the stiffness of the housing to be used when installing the circular spline. Contact us for details of the ratcheting torque.



When ratcheting occurs, the teeth may not be correctly engaged and become out of alignment as shown in Figure 013-1. Operating the drive in this condition will cause vibration and damage the flexspline.



Once ratcheting occurs, the teeth wear excessively and the ratcheting torque may be lowered.



"Dedoidal" condition.

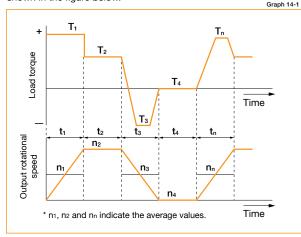
Product Sizing & Selection

In general, a servo system rarely operates at a continuous load and speed. The input rotational speed, load torque change and comparatively large torque are applied at start and stop. Unexpected impact torque may be applied.

These fluctuating load torques should be converted to the average load torque when selecting a model number. As an accurate cross roller bearing is built in the direct external load support (output flange), the maximum moment load, life of the cross roller bearing and the static safety coefficient should also be checked.

■ Checking the application motion profile

Review the application motion profile. Check the specifications shown in the figure below.



Obtain the value of each application motion profile.

Load torque	Tn (Nm)
Time	tn (sec)
Output rotational speed	nn (rpm)

Normal operation pattern

Steady operation
(constant velocity)

T2, t2, n2

Stopping (deceleration)

T3, t3, n3

Maximum rotational speed

Max. output speed no max
Max. input rotational speed ni max
(Restricted by motors)

Emergency stop torque

When impact torque is applied Ts, ts, r

Required life

 $L_{10} = L \text{ (hours)}$

■ Flowchart for selecting a size

Please use the flowchart shown below for selecting a size. Operating conditions must not exceed the performance ratings.

Calculate the average load torque applied on the output side from the application motion profile: Tav (Nm).

$$Tav = \sqrt[3]{\frac{n_1 \cdot t_1 \cdot |T_1|^3 + n_2 \cdot t_2 \cdot |T_2|^3 + \cdots n_n \cdot t_n \cdot |T_n|^3}{n_1 \cdot t_1 + n_2 \cdot t_2 + \cdots n_n \cdot t_n}}$$

Make a preliminary model selection with the following conditions. Tav \leq Limit for average torque torque

(See the rating table of each series).

Calculate the average output speed: no \mathbf{av} (rpm) no $\mathbf{av} = \frac{\mathbf{n_1} \cdot \mathbf{t_1} + \mathbf{n_2} \cdot \mathbf{t_2} + \cdots \cdot \mathbf{n_n} \cdot \mathbf{t_n}}{\mathbf{t_1} + \mathbf{t_2} + \cdots \cdot \mathbf{t_n}}$

Obtain the reduction ratio (R). ni n
A limit is placed on "ni max" by no n

ni *max* no *max* ≧ R

Calculate the average input rotational speed from the average output rotational speed (no *av*) and the reduction ratio (R): ni *av* (rpm)

ni **av** = no **av**·R

Calculate the maximum input rotational speed from the max. output rotational speed (no *max*) and the reduction ratio (R): ni *max* (rpm)

ni *max* = no *max*⋅R

Check whether the preliminary model number satisfies the following condition from the rating table.

Ni $av \leq$ Limit for average speed (rpm)

Ni $\textit{max} \leqq \text{Limit for maximum speed (rpm)}$

OK

Check whether T_1 and T_3 are less than the repeated peak torque specification.

ОК

Check whether $T_{\text{\tiny S}}$ is less than the the momentary peak torque specification.

ОК

Calculate (Ns) the allowable number of rotations during impact torque.

 $N_S = \frac{10^4}{n_S \cdot R} \cdot \dots \cdot N_S \le 1.0 \times 10^4$ $2 \cdot \frac{n_S \cdot R}{60} \cdot t$

JO

Review the operation conditions and model numbe

Calculate the lifetime.

 $L_{10} = 7000 \cdot \left(\frac{\text{Tr}}{\text{Tav}} \right)^3 \cdot \left(\frac{\text{nr}}{\text{ni av}} \right) \text{(hours)}$

Check whether the calculated life is equal to or more than the life of the wave generator (see Page 13).

ОК

The model number is confirmed.

■ Example of model number selection

Value of each application motion profile

Normal operation pattern

Starting (acceleration) T1 = 400 Nm, t1 = 0.3sec, n1 = 7rpm

Steady operation

(constant velocity) T2 = 320 Nm, t2 = 3sec, n2 = 14rpm Stopping (deceleration) T3 = 200 Nm, t3 = 0.4sec, n3 = 7rpm

Dwell $T_4 = 0 \text{ Nm}, t_4 = 0.2 \text{ sec}, n_4 = 0 \text{ rpr}$

Maximum rotational speed

Max. output speed no max = 14 rpm
Max. input speed ni max = 1800 rpm

(Restricted by motors)

Emergency stop torque

When impact torque is applied $T_s = 500 \text{ Nm}$, $t_s = 0.15 \text{ secondary}$

ns = 14 rpm

Required life

 $L_{10} = 7000$ (hours

Calculate the average load torque to the output side based on the application motion profile: Tav (Nm).

$$Tav = \begin{array}{c} 3\sqrt{\frac{7 \text{ rpm} \cdot 0.3 \text{ sec} \cdot |400\text{Nm}|^3 + 14 \text{ rpm} \cdot 3 \text{ sec} \cdot |320\text{Nm}|^3 + 7 \text{ rpm} \cdot 0.4 \text{ sec} \cdot |200\text{Nm}|^3} \\ 7 \text{ rpm} \cdot 0.3 \text{ sec} + 14 \text{ rpm} \cdot 3 \text{ sec} + 7 \text{ rpm} \cdot 0.4 \text{ sec} \end{array}$$

Make a preliminary model selection with the following conditions. Tav = 319 Nm \leq 620 Nm (Limit for average torque for model number CSF-40-120-2A-GR: See the rating table on Page 39.)

Thus, CSF-40-120-2A-GR is tentatively selected.

Calculate the average output rotational speed: no av (rpm)

no
$$av = \frac{7 \text{ rpm} \cdot 0.3 \text{ sec} + 14 \text{ rpm} \cdot 3 \text{ sec} + 7 \text{ rpm} \cdot 0.4 \text{ sec}}{0.3 \text{ sec} + 3 \text{ sec} + 0.4 \text{ sec} + 0.2 \text{ sec}} = 12 \text{ rpm}$$

Obtain the reduction ratio (R).

Calculate the average input rotational speed from the average output rotational speed (no av) and the reduction ratio (R): ni av (rpm)

Calculate the maximum input rotational speed from the maximum output rotational speed (no *max*) and the reduction ratio (R): ni *max* (rpm)

$$\frac{1800 \text{ rpm}}{14 \text{ rpm}} = 128.6 \ge 120$$

ni *max* = 14 rpm·120 = 1680 rpm

Check whether the preliminary selected model number satisfies the following condition from the rating table.

Ni $\it av$ = 1440 rpm \le 3600 rpm (Max average input speed of size 40) Ni $\it max$ = 1680 rpm \le 5600 rpm (Max input speed of size 40)



Check whether T₁ and T₃ are equal to or less than the repeated peak torque specification.

T1 = 400 Nm \leq 617 Nm (Limit of repeated peak torque of size 40) T3 = 200 Nm \leq 617 Nm (Limit of repeated peak torque of size 40)



Check whether Ts is equal to or less than the momentary peak torque specification.

Ts = 500 Nm ≤ 1180 Nm (Limit for momentary torque of size 40)



Calculate the allowable number (Ns) rotation during impact torque and confirm $\leq 1.0 \times 10^4$

$$N_{S} = \frac{10^{4}}{2 \cdot \frac{14 \text{ rpm} \cdot 120}{60}} = 1190 \le 1.0 \times 10^{4}$$



Calculate the lifetime.

$$L_{10} = 7000 \cdot \left(\frac{294 \text{ Nm}}{319 \text{ Nm}}\right)^3 \cdot \left(\frac{2000 \text{ rpm}}{1440 \text{ rpm}}\right) \text{ (hours)}$$

Check whether the calculated life is equal to or more than the life of the wave generator (see Page 12). $L_{10} = 7610 \text{ hours} \geqq 7000 \text{ (life of the wave generator: } L_{10})$



The selection of model number CSF-40-120-2A-GR is confirmed from the above calculations.

Review the operation conditions, size and reduction

NG

Lubrication

Component Sets: CSD-2A, CSF-2A, CSG-2A, F-2, F-0, FR-2, ĀĀ SHF-2A, SHG-2A and SHD and SHG/SHF -2SO and -2SH gear units: Grease lubricant and oil lubricant are available for lubricating the component sets and SHD gear unit. It is extremely important to properly grease your component sets and SHD gear unit. rāoper lubrication is essential for high performance and reliability. Harmonic Drive® component sets are shipped with a rust- preventative oil. The characteristics of the lubricating grease and oil types approved by Harmonic Drive are not changed by mixing with the preservation oil. It is therefore not necessary to remove the preservation oil completely from the gear components. However, the mating surfaces must be degreased before the assembly.

Gear Units: CSG/CSF 2UH and 2UH-LW CSD-2UF and -2UH ĀĀ SHG/SHF-2UH and 2UH- LW SHG/SHF-2UJ CSF Supermini, CSF ĀĀ Mini, and CSF-2UĀ

Grease lubricant is standard for lubricating the gear units. Aou do not need to apply grease during assembly as the product is lubricated

See age 19 for using lubricant beyond the temperaturĀe range in table 16-2.

ontact us if you want consistency zero (NLGI No.0) for maintenance reasons

Name of lubricant Table 016-1 Harmonic Grease® S-1AĀ Harmonic Grease® S-2Ā Grease

Harmonic Grease® 4 No.2Ā Industrial gear oil class-2 (extreme pressure) ISO VG68

Temperature	Table 016-2
	S-1AĀ 0 to + 40ĀĀĀĀ
Grease	S-2Ā 0 to + 40ĀĀĀĀ
	4 No 2Ā =10 to + 70ĀĀĀĀ

ISO VG68 0 to + 40ĀĀĀĀ * The hottest section should not be more than 40° above the ambient temperature.

Note: The three basic components of the gear - the Flexspline, Wave Generator and Circular Spline - are matched and serialized in the factory. Depending on the product they are either greased or prepared with preservation oil. Then the individual components are assembled. If you receive several units, please be careful not to mix the matched components. This can be avoided by verifying that the serial numbers of the assembled gear components are identical.

Grease lubricant

■ Types of lubricant

Harmonic Grease® SK-1A

This grease was developed for Harmonic Drive® gears and features good durability and efficiency.

Harmonic Grease® SK-2

This grease was developed for small sized Harmonic Drive® gears and features smooth rotation of the Wave Generator since high pressure additive is

Harmonic Grease® 4B No.2

This has been developed exclusively for the CSF and CSG and features long life and can be used over a wide range of temperature.

(Note)

- 1. Grease lubrication must have proper sealing, this is essential for 4 No.2.Ā Rotating part: Oil seal with spring is needed. Mating part: O ring or seal adhesive is needed.
- 2. The grease has the highest deterioration rate in the region where the grease is subjected to the greatest shear (near wave generator). Its viscosity is between JIS No.0 and No.00 depending on the operation.

Table 016-3

Table 016-4

NLGI consistency No.	Mixing consistency range
0	355 to 385
00	400 to 430

Grease specification

Table 0							
Grease	SK-1A	SK-2	4B No.2				
ase oilĀ	Refined oil	Refined oil	Composite hydrocarbon oil				
ase VĀiscosity cSt (25)ĀĀ			290 to 320				
Thickening agent	Lithium soap base	Lithium soap base	Urea				
NLGI consistency No.	No. 2	No. 2	No. 1.5				
Additive	Extreme-pressure additive, others	Extreme-pressure additive, others	Extreme-pressure additive, others				
Drop ointĀ	Drop ointĀ 197ĀĀ		247ĀĀ				
Appearance	Yellow	Green	Light yellow				
Storage life	5 years in sealed condition	5 years in sealed condition	5 years in sealed condition				

■ Compatible grease by size

Compatible grease varies depending on the size and reduction ratio. See the following compatibility table. We recommend S-1A and S-2 for general use.ĀĀ

Ratios 30:1

Ratios 30:1 Table 016-5							
Size	8	11	14	17	20	25	32
S-1AĀ	_	_	_	_	0	0	0
S-2Ā	0	0	0	0	_	_	_

Ratios 50:1* and above

4 No.2Ā

Table 016-6

Size	8	11	14	17	20	25	32
S-1AĀ	_	_	_	_	0	0	0
S-2Ā	0	0	0	0	Δ	Δ	Δ
4 No.2Ā	_	_					

Size	40	45	50	58	65	80	90	100
S-1AĀ	0	0	0	0	0	0	0	0
S-2Ā	Δ	_	_	_	_	_	_	-
4No.2Ā								

- Semi-standard grease
- Recommended grease for long life and high load
- Oil lubrication is required for component-sets size 50 or larger with a reduction ratio of 50:1.

Grease characteristics

Table 016 7

Grease orial acteristics	Table 016-7		
Grease	SK-1A	SK-2	4B No.2
Durability	0	0	0
Fretting resistance	0	0	0
Low-temperature performance	Δ	Δ	0
Grease leakage	0	0	Δ

Use Caution :△

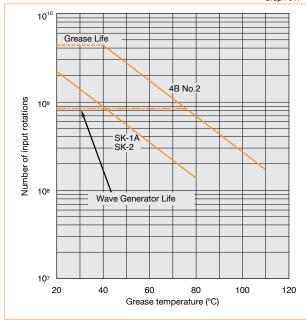
■ When to replace grease

The wear characteristics of the gear are strongly influenced by the condition of the grease lubrication. The condition of the grease is affected by the ambient temperature. The graph 017-1 shows the maximum number of input rotations for various temperatures. This graph applies to applications where the average load torque does not exceed the rated torque.

Note: Recommended Grease: S-1A or S-2ĀĀ

When to replace grease: LGTn (when the average load torque is equal to or less than the rated torque)





Calculation formula when the average load torque exceeds the rated torque

Formula 017-1

$$L_{GT} = L_{GTn} \times \left(\frac{Tr}{Tav}\right)^3$$

Formu	la Qı	ıml	പ	e
1 Ollilla	ia o	y 1 1 11	JUI	0

1 Official	Table 017-1						
La	Grease change (if average load input torque exceeds rated torque) revolutions						
L _{GTn}	Grease change (if average load torque is equal to or less than rated torque)	input revolutions (From Graph)	See the Graph 017-1.				
Tr	Rated torque	Nm	See the atings TĀĀableĀĀ of each series.				
Tav	Average load torque	Nm	Calculation formula: See age 014.Ā				

■ Other precautions

- 1. Avoid mixing different kinds of grease. The gear should be in an individual case when installed.
- lease contact us when you use HarmonicDriveĀ® gears at constant load or in one direction continuously, as it may cause lubrication problems.
- Grease leakage. A sealed structure is needed to maintain the high durability of the gear and prevent grease leakage.
- See the corresponding pages of the design guide of each series for ecommended ĀĀ minimum housing clearance, Application guideand pplication quantity ĀĀĀĀĀĀ

Engineering Data

Precautions on using Harmonic Grease® 4B No.2

Harmonic Grease® 4B No.2 lubrication is ideally suited for Harmonic Drive® gears.

- (1) Apply the grease to each contacting joint at the beginning of operation.
- (2) Remove any contaminents created by abrasion during running-in period.
- See the corresponding pages of the design guide of each series for "recommended minimum housing clearance," Application guide" and "Application quantity."

■ Precautions

(1) Stir Grease

When storing Harmonic Grease 4B No.2 lubrication in the container, it is common for the oil to weep from the thickener. Before greasing, stir the grease in the container to mix and soften.

(2) Aging (running-in)

The aging before the main operation softens the applied grease. More effective greasing performance can be realized when the grease is distributed around each contact surface.

Therefore, the following aging methods are recommended.

- Keep the internal temperature at 80°C or cooler. Do not start the aging at high temperature rapidly.
- Input rotational speed should be 1000rpm to 3000rpm. However, the lower rotational speed of 1000rpm is more effective.
 Set the speed as low as possible within the indicated range.
- The time required for aging is 20 minutes or longer.
- · Operation range for aging: Keep the output rotational angle as large as possible.

Contact us if you have any questions for handling Harmonic Grease 4B No.2 lubrication.

Note: Strict sealing is required to prevent grease leakage.

Oil lubricant

■ Types of oil

The specified standard lubricant is "Industrial gear oil class-2 (extreme pressure) ISO VG68." We recommend the following brands as a commercial lubricant.

Table 018-1

Standard	Mobil Oil	Exxon	Shell	COSMO Oil	Japan Energy	NIPPON Oil	Idemitsu Kosan	General Oil	Klüber
Industrial gear oil class-2 (extreme pressure) ISO VG68	Mobilgear 600XP68	Spartan EP68	Omala Oil 68	Cosmo gear SE68	ES gear G68	Bonock M68, Bonock AX68	Daphne super gear LW68	General Oil SP gear roll 68	Syntheso D-68EP

■ When to replace oil

See the corresponding pages of the design guide of each series for specific details.

■ Other precautions

- 1. Avoid mixing different kinds of oil. The gear should be in an individual case when installed.
- 2. When you use size 50 or above at max allowable input speed, please contact us as it may cause lubrication problems.
- * Oil lubrication is required for component-sets size 50 or larger with a reduction ratio of 50:1.

Lubricant for special environments

When the ambient temperature is special (other than the "temperature range of the operating environment" on Page 016-2), you should select a lubricant appropriate for the operating temperature range.

Harmonic Grease 4B No.2

Table 019-1

Type of lubricant	Operating temperature range	Available temperature range	
Grease	-10°C to + 110°C	−50°C to + 130°C	

High temperature lubricant

Table 019-2

Type of lubricant	Lubricant and manufacturer	Available temperature range
Grease	Mobil grease 28: Mobil Oil	−5°C to + 160°C
Oil	Mobil SHC-626: Mobil Oil	−5°C to + 140°C

Low temperature lubricant

Table 019-3

Type of lubricant	Lubricant and manufacturer	Available temperature range
Grease	Multemp SH-KII: Kyodo Oil	−30°C to + 50°C
Grease	Isoflex LDS-18 special A: KLÜBER	−25°C to + 80°C
0.1	SH-200-100CS: Toray Silicon	-40°C to + 140°C
Oil	Syntheso D-32EP: KLÜBER	-25°C to + 90°C

Harmonic Grease 4B No.2

The operating temperature range of Harmonic Grease 4B No.2 lubrication is the temperature at the lubricating section with the performance and characteristics of the gear taken into consideration. (It is not ambient temperature.)

As the available temperature range indicates the temperature of the independent lubricant, restriction is added on operating conditions (such as load torque, rotational speed and operating cycle) of the gear. When the ambient temperature is very high or low, materials of the parts of the gear need to be reviewed for suitability. Contact us if operating in high temperature.

Harmonic Grease 4B No.2 can be used in the available temperature range shown in table 019-1. However, input running torque will increase at low temperatures, and grease life will be decreased at high temperatures due to oxidation and lubricant degradation.

Torsional Stiffness

Stiffness and backlash of the drive system greatly affects the performance of the servo system. Please perform a detailed review of these items before designing your equipment and selecting a model number.

■ Stiffness

Fixing the input side (wave generator) and applying torque to the output side (flexspline) generates torsion almost proportional to the torque on the output side. Figure 018-1 shows the torsional angle at the output side when the torque applied on the output side starts from zero, increases up to +To and decreases down to -To. This is called the "Torque – torsion angle diagram," which normally draws a loop of 0-A-B-A'-B'-A. The slope described in the "Torque – torsion angle diagram" is represented as the spring constant for the stiffness of the HarmonicDrive® gear (unit: Nm/rad).

As shown in Figure 020-1, this "Torque – torsional angle diagram" is divided into 3 regions, and the spring constants in the area are represented by K_1 , K_2 and K_3 .

 K_1 The spring constant when the torque changes from [zero] to [T₁] K_2 The spring constant when the torque changes from [T₁] to [T₂]

K₃ ···· The spring constant when the torque changes from [T₂] to [T₃]

See the corresponding pages of each series for values of the spring constants (K₁, K₂, K₃) and the torque-torsional angles (T₁, T₂, - θ₁, θ₂).

■ Example for calculating the torsion angle

The torsion angle (θ) is calculated here using CSF-25-100-2A-GR as an example.

When the applied torque is T_1 or less, the torsion angle θ_{L1} is calculated as follows:

When the load torque T_{L1} =2.9 Nm θ_{L1} = T_{L1}/K_1 = 2.9/3.1×10⁴

=9.4×10⁻⁵ rad (0.33 arc min)

When the applied torque is between T_1 and T_2 , the torsion angle θ_{12} is calculated as follows:

When the load torque is TL2=39 Nm

 $\theta_{L2} = \theta_1 + (T_{L2} - T_1)/K_2$ = $4.4 \times 10^{-4} + (39-14)/5.0 \times 10^{4}$ = 9.4×10^{-4} rad (3.2 arc min)

When a bidirectional load is applied, the total torsion angle will be 2 x θ_{LX} plus hysteresis loss.

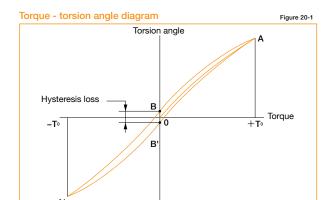
* The torsion angle calculation is for the gear component set only and does not include any torsional windup of the output shaft.

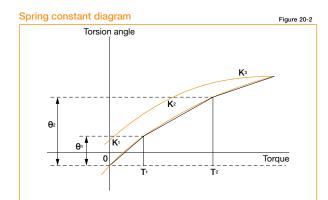
Note: See p.120 for torsional stiffness for pancake gearing.

■ Hysteresis loss (Silk hat and cup style only)

As shown in Figure 020-1, when the applied torque is increased to the rated torque and is brought back to [zero], the torsional angle does not return exactly back to the zero point This small difference $(B-B^{\prime})$ is called hysteresis loss.

See the corresponding page of each series for the hysteresis loss value.





■ Backlash (Silk hat and cup style only)

Hysteresis loss is primarily caused by internal friction. It is a very small value and will vary roughly in proportion to the applied load. Because HarmonicDrive® gears have zero backlash, the only true backlash is due to the clearance in the Oldham coupling, a self-aligning mechanism used on the wave generator. Since the Oldham coupling is used on the input, the backlash measured at the output is extremely small (arc-seconds) since it is divided by the gear reduction ratio.

Positional Accuracy

Positional Accuracy values represent the difference between the theoretical angle and the actual angle of output for any given input. The values shown in the table are maximum values.

See the corresponding pages of each series for transmission accuracy values.

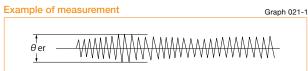


	Table 021-1
θ er	Transmission accuracy
θ,	Input angle
θ_{z}	Actual output angle
R	Reduction ratio



Vibration

The primary frequency of the transmission error of the HarmonicDrive® gear may cause a vibration of the load inertia. This can occur when the driving frequency of the servo system including the HarmonicDrive® gear is at, or close to the resonant frequency of the system. Refer to the design guide of each series.

The primary component of the transmission error occurs twice per input revolution of the input. Therefore, the frequency generated by the transmission error is 2x the input frequency (rev / sec).

If the resonant frequency of the entire system, including the HarmonicDrive® gear, is F=15 Hz, then the input speed (N) which would generate that frequency could be calculated with the formula below.

Formula 021-2

$$N = \frac{15}{2} \cdot 60 = 450 \text{ rpm}$$

The resonant frequency is generated at an input speed of 450 rpm.

How to the calculate resonant frequency of the system

Formula 021-3 $f = \frac{1}{2\pi} \sqrt{\frac{K}{J}}$

Formula	a variables		Table 021-2
f	The resonant frequency of the system	Hz	
K	Spring constant	Nm/rad	See pages of each series
J	Load inertia	kgm²	

Starting Torque

Starting torque is the torque value applied to the input side at which the output first starts to rotate. The values in the table of each series indicate the maximum value, and the lower-limit value indicates approximately $^{1}\!/_{2}$ to $^{1}\!/_{3}$ of the maximum value.

Measurement conditions:

No-load, ambient temperature: +20°C

- See the corresponding pages of each series for starting torque values.
- * Use the values in the table of each series as reference values as they vary depending on the usage conditions

Backdriving Torque

Backdriving torque is the torque value applied to the output side at which the input first starts to rotate. The values in the table are maximum values, typical values are approximately $^1\!/_2$ of the maximum values.

Note: Never rely on these values as a margin in a system that must hold an external load. A brake must be used where back driving is not permissible.

Measurement conditions:

No-load, ambient temperature: +20°C

- See the corresponding pages of each series for backdriving torque values.
- * Use the values in the table of each series as reference values as they vary depending on the usage conditions.

No-Load Running Torque

No-load running torque is the torque which is required to rotate the input side (high speed side), when there is no load on the output side (low speed side). The graph of the no-load running torque shown in this catalog depends on the measurement conditions shown in Table 023-1.

Add the compensation values shown by each series to all reduction ratios except 100:1.

See the corresponding pages of each series for no-load running torque values.

Measurement condition

Table 023-1

Reduction ratio 100					
			Harmonic Grease SK-1A		
Lubricant	Grease Jubrication	Name	Harmonic Grease SK-2		
labrication		Quantity	(See pages of each series)		
Torque value is measured after 2 hours at 2000 rpm input					

^{*} Contact us for oil lubrication.

Efficiency

The efficiency varies depending on the following conditions.

- Reduction ratio
- Input speed
- Load torque
- Temperature
- Lubrication (type and quantity)

The efficiency characteristics of each series shown in this catalog depends on the measurement condition shown in Table 023-2.

See the corresponding pages of each series for efficiency values.

■ Efficiency compensation coefficient

If load torque is below rated torque, a compensation factor must be employed. Calculate the compensation coefficient Ke from the efficiency compensation coefficient graph of each series and use the following example for calculation.

Example of calculation

Efficiency η (%) under the following condition is obtained from the example of CSF-20-80-2A-GR.

Input rotational speed: 1000 rpm

Load torque: 19.6 Nm

Lubrication method: Grease lubrication (Harmonic Grease SK-1A) Lubricant temperature: 20°C

Since the rated torque of size 20 with a reduction ratio of 80 is 34 Nm (Ratings: Page 039), the torque ratio α is 0.58. (α =19.6/34=0.58)

- The efficiency compensation coefficient is Ke=0.93 from Graph 023-1.
- Efficiency η at load torque 19.6 Nm: η=Ke⋅ηR=0.93 x 78=73%

Measurement condition

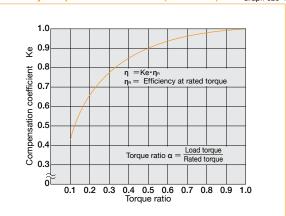
Table 023-2

Installation	Based on recommended tolerance		
Load torque	The rated torque shown in the rating table (see the corresponding pages on each series)		
		Name	Harmonic Grease SK-1A
Lubricant	Grease		Harmonic Grease SK-2
Lubricani	Lubrication Quant		Recommended quantity (see the pages on each series)

^{*} Contact us for oil lubrication

Efficiency compensation coefficient (CSF series)

Graph 023-1



^{*} Efficiency compensation coefficient Ke=1 when the load torque is greater than the rated torque.

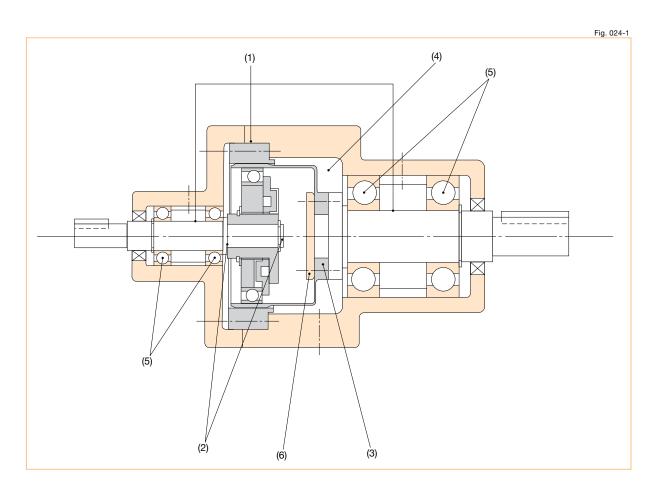
Design Guidelines

Design guideline

The relative perpendicularity and concentricity of the three basic Harmonic Drive® elements have an important influence on accuracy and service life.

Misalignments will adversely affect performance and reliability. Compliance with recommended assembly tolerances is essential in order for the advantages of Harmonic Drive® gearing to be fully realized. Please consider the following when designing:

- (1) Input shaft, Circular Spline and housing must be concentric.
- (2) When operating, an axial force is generated on the wave generator. Input bearings must be selected to accommodate this axial load. See page 27.
- (3) Even though a HarmonicDrive® gear is compact, it transmits large torques. Therefore, assure that all required bolts are used to fastened the circular spline and flexspline and that they are tightened to the recommended torque.
- (4) As the flexspline is subject to elastic deformation, the A minimal clearance between the flexspline and housing is required. Refer to "Minimum Housing Clearance" on the drawing dimension tables.
- (5) The input shaft and output shaft are supported by anti-friction bearings. As the wave generator and flexspline elements are meant to transmit pure torque only, the bearing arrangement needs to isolate the harmonic gearing from external forces applied to either shaft. A common bearing arrangement is depicted in the diagram.
- (6) A clamping plate is recommended (item 6). Its purpose is to spread fastening forces and to avoid any chance of making physical contact with the thin section of the flexspline diaphragm. The clamping plate shall not exceed the diaphragm's boss diameter and is to be designed in accordance with catalog recommendations.

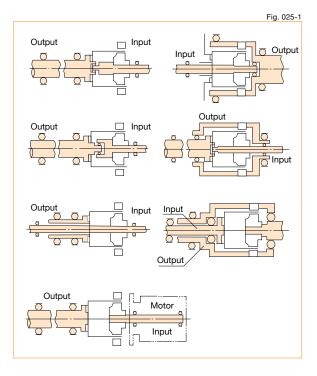


Bearing support for the input and output shafts

For the component sets, both input and output shafts must be supported by two adequately spaced bearings in order to withstand external radial and axial forces without excessive deflection. In order to avoid damage to the component set when limited external loads are anticipated, both input and output shafts must be axially fixed.

Bearings must be selected whose radial play does not exceed ISO-standard C 2 class or "normal" class. The bearings should be axially and radially preloaded to eliminate backlash.

Examples of correct bearing arrangements are shown in fig 025-1.

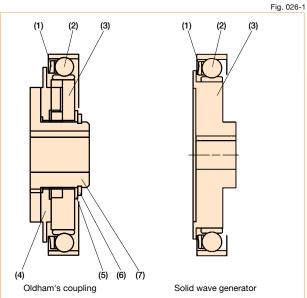


Wave generator

■ Structure of the wave generator

The wave generator includes an Oldham's coupling type with a self-aligning structure and an integrated solid wave generator without a self-aligning structure, and which is used depends on the series.

See the diagram of each series for details. The basic structure of the wave generator and the shape are shown below.



- (1) Ball Separator
- (2) Wave generator bearing
- (3) Wave generator plug
- (4) Insert
- (5) Rubwasher
- (6) Snap ring
- 7) Wave generator hub

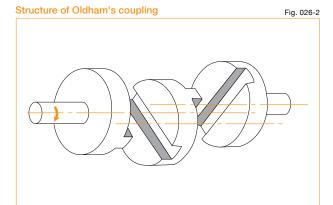


Table 027-1

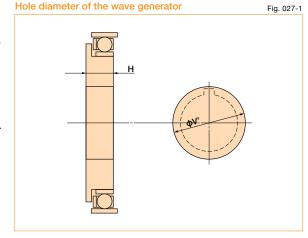
■ Maximum hole diameter of wave generator

The standard hole dimension of the wave generator is shown for each size. The dimension can be changed within a range up to the maximum hole dimension. We recommend the dimension of keyway based on JIS standard. It is necessary that the dimension of keyways should sustain the transmission torque.

ed holes are also availabl

In cases where a larger hole is required, use the wave generator without the Oldham coupling. The maximum diameter of the hole should be considered to prevent deformation of the Wave Generator plug by load torque. The dimension is shown in the table below and includes the dimension of depth of keyway.

(This is the value including the dimension of the depth of keyway.)



of the wave generator but with Oldham countin

Hole diameter of the wave generator hub with Oldnam coupling										Unit: mm					
Size	8	11	14	17	20	25	32	40	45	50	58	65	80	90	100
Standard dim. (H7)	3	5	6	8	9	11	14	14	19	19	22	24	28	28	28
Minimum hole dim.	_	_	3	4	5	6	6	10	10	10	13	16	16	19	22
Maximum hole dim.	_	_	8	10	13	15	15	20	20	20	25	30	35	37	40

Maximum hole	diamete	er withou	ut Oldha	ım Coup	oling									T	able 027-2 Unit: mm
Size	8	11	14	17	20	25	32	40	45	50	58	65	80	90	100
Max. hole dia.φV'	10	14	17	20	23	28	36	42	47	52	60	67	72	84	95
Min. plug thick.H _{-0.1}	5.7	6.7	7.2	7.6	11.3	11.3	13.7	15.9	17.8	19	21.4	23.5	28.5	31.3	34.9

Axial Force of Wave Generator

When the gear is used to accelerate a load, the deflection of the Flexspline leads to an axial force acting on the Wave Generator. This axial force, which acts in the direction of the closed end of the Flexspline, must be supported by the bearings of the input shaft (motor shaft). When the gear is used to decelerate a load, an axial force acts to push the Wave Generator out of the Flexspline cup. Maximum axial force of the Wave Generator can be calculated by the equation shown below. The axial force may vary depending on its operating condition. The value of axial force tends to be a larger number when using high torque, extreme low speed and constant operation. The force is calculated (approximately) by the equation. In all cases, the Wave Generator must be axially (in both directions), as well as torsionally, fixed to the input shaft.

Please contact us for further information on attaching the Wave Generator to the input (motor) shaft.

Axial force direction of the wave generator Fig. 027-2 direction for direction for Axial Axial force in force in deceleration acceleration

Formula for Axial Force

Reduction ratio	Calculation formula
30	F=2×-Tx0.07×tan 32°
50	F=2×-Tx0.07×tan 30°
80 or more	F=2×-Tx0.07×tan 20°

Symbols for Formula

Table 027-4

	,			Tubic of 1
F	=	Axial force	N	See Figure 027-2
)	Size	m	
Г	Г	Output torque	Nm	

Calculation example

Formula 027-1

Model name: **CSF** series 32 Size: Reduction ratio: 50 Output torque: 382 Nm

(maximum allowable momentary torque)

$$F=2\times \frac{382}{(32\times 0.00254)}\times 0.07\times \tan 30^{\circ}$$

F=380N

Assembly Precautions

Sealing

Sealing is needed to maintain the high durability of the gear and prevent grease leakage. Recommended for all mating surfaces, if the o-ring is not used. Flanges provided with o-ring grooves must be sealed when a proper seal cannot be achieved using the o-ring alone.

 Rotating Parts 	 Oil seal with spring is
	needed.
 Mating flange 	 O-ring or seal adhesive is
	needed.
· Screw hole area	 Screws should have a thread
	lock (LOCTITE® 242 is
	recommended) or seal
	adhesive.

(Note) If you use Harmonic Grease 4BNo.2, strict sealing is required.

O !!		4 44	_	
Spaling	recommen	datione	tor apar	' i inite

Table 028-

Area requiring sealing		Recommended sealing method			
Output	Holes which penetrate housing	Use O-ring (supplied with the product)			
side	Installation screw / bolt	Screw lock adhesive which has effective seal (LOCTITE® 242 is recommended)			
	Flange surfaces	Use O-ring (supplied with the product)			
Input side	Motor output shaft	Please select a motor which has an oil seal on the output shaft.			

Assembly precautions

The wave generator is installed after the flexspline and circular spline. If the wave generator is not inserted into the flexspline last, gear teeth scuffing damage or improper eccentric gear mesh may result. Installation resulting in an eccentric tooth mesh (Dedoidal) will cause noise and vibration, and can lead to early failure of the gear. For proper function, the teeth of the flexspline and Circular Spline mesh symmetrically.

■ Precautions on the wave generator

- Avoid applying undue axial force to the wave generator during installation. Rotating the wave generator bearing while inserting it is recommended and will ease the process.
- If the wave generator does not have an Oldham coupling, extra care must be given to ensure that concentricity and inclination are within the specified limits

Precautions on the circular spline

The circular Spline must not be deformed in any way during the assembly. It is particularly important that the mounting surfaces are prepared correctly

- Mounting surfaces need to have adequate flatness, smoothness, and no distortion.
- Especially in the area of the screw holes, burrs or foreign matter should not be present.
- 3. Adequate relief in the housing corners is needed to prevent interference with the corner of the circular spline.
- The circular spline should be rotatable within the housing. Be sure there is not interference and that it does not catch on anything.
- When a bolt is inserted into a bolt hole during installation, make sure that the bolt fits securely and is not in an improper position or inclination.
- 6. Do not apply torque at recommended torque all at once. First, apply torque at about half of the recommended value to all bolts, then tighten at recommended torque. Order of tightening bolts must be diagonal.
- Avoid pinning the circular spline if possible as it can reduce the rotational precision and smoothness of operation.

■ Precautions on the flexspline

- Mounting surfaces need to have adequate flatness, smoothness, and no distortion.
- Especially in the area of the screw holes, burrs or foreign matter should not be present.
- Adequate clearance with the housing is needed to ensure no interference especially with the major axis of flexspline
- 4. Bolts should rotate freely when installing through the mounting holes of the flexspline and should not have any irregularity due to the shaft bolt holes being misaligned or oblique.
- 5. Do not tighten the bolts with the specified torque all at once. Tighten the bolts temporarily with about half the specified torque, and then tighten them to the specified torque. Tighten them in an even, crisscross pattern.
- The flexspline and circular spline are concentric after assembly. After installing the wave generator bearing, if it rotates in unbalanced way, check the mounting for dedoidal or non-concentric installation.
- Care should be taken not to damage the flexspline diaphragm or gear teeth during assembly.
 - Avoid hitting the tips of the flexpline teeth and circular spline teeth. Avoid installing the CS from the open side of the flexspline after the wave generator has been installed.

■ Rust prevention

Although the Harmonic Drive® gears come with some corrosion protection, the gear can rust if exposed to the environment. The gear external surfaces typically have only a temporary corrosion inhibitor and some oil applied. If an anti-rust product is needed, please contact us to review the options.

"Dedoidal" state

It is normal for the flexspline to engage with the circular spline symmetrically as shown in Figure 029-1. However, if the ratcheting phenomenon, which is described on Page 013, is caused or if the three parts are forcibly inserted and assembled, engagement of the teeth may be out of alignment as shown in Figure 029-2. This is called "dedoidal". Note: Early failure of the gear will occur.

■ How to check "dedoidal"

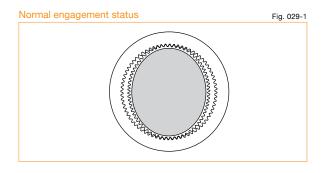
By performing the following methods, check whether the gear engagement is "dedoidal".

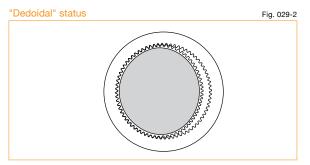
(1) Judging by the irregular torque generated when the wave generator turns

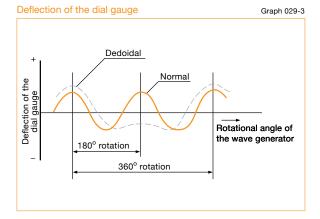
- Slowly turn the input shaft with your hand in a no-load condition. If you can turn it with average force, it is normal. If it turns irregularly, it may be "dedoidal".
- 2) Turn the wave generator in a no-load condition if it is attached to a motor. If the average current value of the motor is about 2 to 3 times the normal value, it may be "dedoidal".

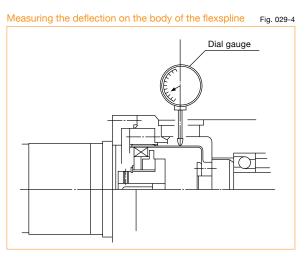
(2) Judging by measuring vibration on the body of the flexspline

The scale deflection of the dial gauge draws a sine wave as shown by the solid line in Graph 029-3 when it is normally assembled. When "dedoidal" occurs, the gauge draws a deflected wave shown by the dotted line as the flexspline is out of alignment.









Checking Output Bearing:

A precision cross roller bearing is built in the unit type and the gear head type to directly support the external load (output flange) (precision 4-point contact ball bearing for the CSF-mini series).

lease calculate maximum moment load, life of crāoss roller bearing, and static safety factor to fully maximize the performance of a housed unit

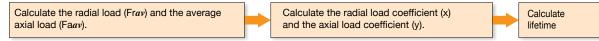
See the corresponding pages on each series for cross roller bearing specifications.

Checking procedure

(1) Checking the maximum moment load (Mmax)



(2) Checking the life



(3) Checking the static safety coefficient



How to calculate the maximum moment load

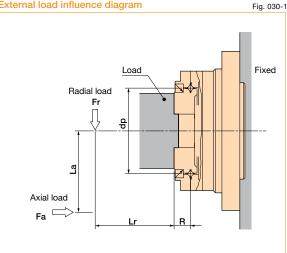
Maximum moment load (Mmax) is obtained as follows. Make sure that $Mmax \leq Mc$.

Formula 030-1 $M max = Frmax (Lr+R) + Famax \cdot La$

Symb	ools f	or F	ormul	la 0	30-1
------	--------	------	-------	------	------

Symbols	for Formula 030-1		Table 030-1
Frmax	Max. radial load	N(kgf)	See Fig. 030-1.
Fa <i>max</i>	Max. axial load	N(kgf)	See Fig. 030-1.
Lr, La		m	See Fig. 030-1.
R	Offset amount	m	See Fig. 030-1 and pecification of ĀĀ the output bearingof each series. ĀĀ

External load influence diagram



How to calculate the average load

(Average radial load, average axial load, average output speed)

When the radial load and axial load vary, the life of cross roller bearing can be determined by converting to an average load.

How to calculate the average radial load (Frav)

Formula 031-1

(Cross roller bearing)

Fr
$$av = \sqrt[1003]{\frac{n_1t_1(|Fr_1|)^{10/3} + n_2t_2(|Fr_2|)^{10/3} \cdots + n_nt_n(|Fr_n|)^{10/3}}{n_1t_1 + n_2t_2 \cdots + n_nt_n}}$$

(4-point contact ball bearing)

Fr
$$av = \sqrt[3]{\frac{n_1t_1(|\mathsf{Fr_1}|)^3 + n_2t_2(|\mathsf{Fr_2}|)^3 \cdots + n_nt_n(|\mathsf{Fr_n}|)^3}{n_1t_1 + n_2t_2\cdots + n_nt_n}}$$

Note that the maximum radial load in t₁ is Fr₁ and the maximum radial load in t₃ is Fr₃.

How to calculate the average axial load (Faav)

Formula 031-2

(Cross roller bearing)

Fa
$$av = \sqrt[103]{\frac{n_1t_1(|Fa_1|)^{10/3} + n_2t_2(|Fa_2|)^{10/3} \cdots + n_nt_n(|Fa_n|)^{10/3}}{n_1t_1 + n_2t_2 \cdots + n_nt_n}}$$

(4-point contact ball bearing)

Fa
$$av = \sqrt[3]{\frac{n_1t_1(|Fa_1|)^3 + n_2t_2(|Fa_2|)^3 \cdots + n_nt_n(|Fa_n|)^3}{n_1t_1 + n_2t_2 \cdots + n_nt_n}}$$

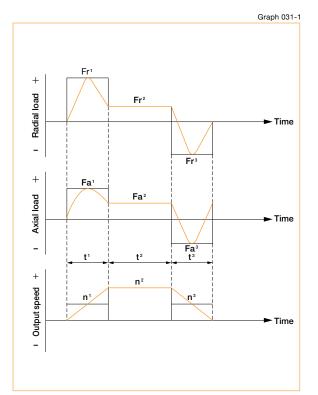
Note that the maximum axial load in t₁ is Fa₁ and the maximum axial load in t₃ is Fa₃.

How to calculate the average output speed

(Nav)

Formula 031-3

$$N av = \frac{n_1 t_1 + n_2 t_2 \ n \bar{A} \bar{A}_{-n} t_n}{t_1 + t_2 \ t \bar{A} \bar{A}_{-n}}$$



How to calculate the radial load coefficient (X) and axial load coefficient (Y)

Formula 031-4

How to calculate the load coefficient	t	Х	Υ
Faav Frav+2 (Frav (Lr+R) + Frav • La) /dp	=1.5Ā	1	0.45
Faav Frav+2 (Frav (Lr+R) + Frav • La) /dp	1.5Ā	0.67	0.67

Symbols for Formula 031-4

|--|

-			
Frav	Average radial load	N(kgf)	See ow to calculate the averageĀĀ load.See Formula 031-1.ĀĀ
Faav	Average axial load	N(kgf)	See ow to calculate the averageĀĀ load.See Formula 031-2.ĀĀ
Lr, La		m	See fig. 030-1
R	Offset amount	m	See Fig. 030-1 and ain rĀĀoller bearing specificationsof each seriesĀĀ
dp	itch cirĀcle diameter of a roller	m	See Fig. 030-1 and pecification of ĀĀ the output bearingof each series.ĀĀ

Life of the output bearing

Calculate life of the output bearing by Formula 032-1. You can calculate the dynamic equivalent radial load (Pc) by Formula 032-2.

Formula 032-1

(Cross roller bearing)

$$L_{10} = \frac{10^6}{60 \times N \text{ av}} \times \left(\frac{C}{\text{fw} \cdot \text{Pc}}\right)^{10/3}$$

(4-point contact ball bearing)

$$L_{10} = \frac{10^6}{60 \times N \text{ av}} \times \left(\frac{C}{\text{fw} \cdot \text{Pc}}\right)^3$$

Symbols for Formula 032-1

Table 032-1

0,	7 101 1 011111010 002 1	Table 052-1	
L ₁₀	Life	hour	
Nav	Average output rated load speed	rpm	See "How to calculate the average load."
С	Basic dynamic rated load	N (kgf)	See "Specification of the output bearing" of each series.
Pc	Dynamic equivalent	N (kgf)	See Formula 032-2.
fw	Load coefficient		See Table 032-3.

Formula 032-2

$$Pc = X \cdot \left(Frav + \frac{2(Frav (Lr+R) + Frav \cdot La)}{dp} \right) + Y \cdot Faav$$

Symbols	ymbols for Formula 032-2		Table 032-2
Frav	Average radial load	N (kgf)	See "How to calculate the average load." See Formula 031-1.
Faav	Average axial load	N (kgf)	See "How to calculate the average load." See Formula 031-2.
dp	Pitch circle diameter	m	See Fig. 030-1 and "Specification of the output bearing" of each series.
х	Radial load coefficient		See Formula 031-4.
Y	Axial load coefficient		See Formula 031-4.
Lr, La		m	See Figure 030-1.
R	Offset	m	See Fig. 030-1 and "Specification of the output bearing" of each series.
M ave	Average moment load	Nm	

Load coefficient

Table 032-3

Load status	fw
Steady operation without impact and vibration	1 to 1.2
Normal operation	1.2 to 1.5
Operation with impact and vibration	1.5 to 3

Fig. 033-1

How to calculate life during oscillating motion

Formula 033-1

(Cross roller bearing)

$$Loc = \frac{10^6}{60 \times n1} \times \frac{90}{\theta} \times \left(\frac{C}{\text{fw} \cdot \text{Pc}}\right)^{10/3}$$

(4-point contact ball bearing)

$$Loc = \frac{10^6}{60 \times n1} \times \frac{90}{\theta} \times \left(\frac{C}{\text{fw} \cdot \text{Pc}}\right)^3$$

Symbols for Formula 033-1

Table 033-1

Cymbols for Formula 000-1				lable 033-
L	oc.	Rated life for oscillating motion	hour	
	n1	Round trip oscillation each minute	срт	
	С	Basic dynamic rated load	N (kgf)	
ı	Pc	Dynamic equivalent radial load	N (kgf)	See Formula 032-2.
1	fw	Load coefficient		See Table 032-3.
	θ	Oscillating angle /2	Degree	See Fig. 033-1.

Oscillating angle

(Note) A small angle of oscillation (less than 5 degrees) may cause fretting corrosion to occur since lubrication may not circulate properly. Contact us if this happens.

How to calculate the static safety coefficient

Basic static rated load is an allowable limit for static load, but its limit is determined by usage. In this case, static safety coefficient of the cross roller bearing can be calculated by Formula 034-2.

Formula 034-1

Formula 034-2
$$0 = \overline{A}Fr max + \frac{2M max}{1} + 0.44Fa max$$

dp

-+0.44Fa *max*

Symbols for Formula 034-1			Table 034-
Co	Basic static rated load	N(kgf)	See "Specification of the output bearing" of each series.
Po	Static equivalent radial load	N(kgf)	See Formula 034-2.

Static Safety Coefficient

otatic daicty docincient	Table 034-3
Operating condition of the roller bearing	fs
When high rotation precision is required	≧3
When shock and vibration are expected	≧2
Under normal operating condition	≧1.5

Symbols for Formula 034-2

Table 034-2

O y 11110011	5 101 1 01111ala 00 1 E	Tubic 00+ L	
Frmax	Max. radial load	N(kgf)	
Famax	Max. axial load	N(kgf)	
Mmax	Max. moment load	Nm(kgfm)	
dp	Pitch circle diameter of a roller	m	See Fig. 030-1 and "Specification of the output bearing" of each series.



HarmonicDrive® Reducer for Precision Control

For Safe Use of Harmonic Drive® Component Set and Gear Unit

Warning: Means that improper use or handling could result in a risk of death or serious injury.

: Means that improper use or handling could result in personal injury or damage to property.

Limited Applications

This product cannot be used for the following applications:

- * Space equipment
- * Aircraft equipment
- * Nuclear power equipment
- Equipment and apparatus used in domestic homes

- * Vacuum equipment
- * Automotive equipment Game equipment
- * Equipment that directly works on human bodies

- * Equipment for transport of humans
- Equipment for use in a special environment

Please consult Harmonic Drive beforehand when intending to use one of its product for the aforementioned applications.

Install a safety device that avoids an accident even if output of this product becomes uncontrollable due to breakdown when using it in equipment that affects human lives and that may trigger serious damage.

Design Precaution: Be certain to read the catalog when designing your equipment. Install the equipment in a specified manner. Use only in a specified environment. Carry out assembly precisely in the specified order according to Please ensure the following environmental conditions are the catalog. complied with: Observe our recommended tightening methods (such as bolts Ambient temperature 0 to 40°C No splashing of water or oil Caution Caution Operating the equipment without precise assembly can cause · Do not expose to corrosive or explosive gas troubles such as generation of vibration, reduction of life, No dust such as metal powder deterioration of precision and breakdown. Use the specified lubricant. Install the equipment in a specified precision. Using other lubricant than our recommended products can Design and assemble parts to maintain the recommended reduce the life. Replace the lubricant in a specified installation and assembly tolerances in the catalog. condition. Failure to keep the precision can cause troubles such as Grease is sealed in a unit product. Do not mix other kinds of Caution vibration, reduction of life, deterioration of precision and Caution grease. breakdown

Operational Precaution: Be certain to read the catalog before operating the equipment. Be careful in handling products and parts. Apply torque within the allowable range. Do not impact the parts and units with a hammer, etc. Do not scratch or dent them. Possible damage is assumed. Do not apply torque exceeding the instantaneous allowable max. torque. Applying excess torque can cause troubles such as loose If you use the equipment in a damaged condition, the specified tightening bolts, generation of backlash and breakdown. performance may not be retained. It can also cause troubles Striking an arm directly attached to the output shaft can damage Caution Caution such as breakdown the arm and make the output shaft uncontrollable.



Do not change a set of parts.

- The product is manufactured with matched serial numbers. The specified performance may not be retained if you have used mixed sets of parts.
- Rust-proofing was applied before shipping. However, please note that rusting occurs earlier depending on the customers' storage environment.

Caution

Do not break down unit products.

 Do not break down and reassemble unit products. Original performance may not be reproduced.



- - Although black oxide finish is applied to some of our products, it dose not guarantee the antirust effect.

Handling lubricant



Precautions on handling lubricant

- Use protective eyewear when handling. Avoid contact with eyes. May cause inflammation.
- Use gloves and other skin protection when handling. Avoid contact with skin. May cause inflammation.
- Do not swallow. May cause diarrhea and vomiting.
- Keep out of reach of children.

Treatment of waste oil and containers

- $\hfill \square$ Proper disposal is essential. Dispose of waste oil and waste containers properly in accordance with applicable laws and regulations.
- Do not apply pressure on an empty container.
- Do not weld, heat, drill or cut the container. The remainder may ignite with an explosion.

First-aid



- EYES: Flush with clean water for at least 15 minutes. Consult a physician.
- SKIN: Thoroughly remove with cloth or paper and wash with soap and water.
- NGESTION: Consult a physician immediately. Do not induce vomiting.
- INHALATION: Immediately seek fresh air if adverse effects are observed

Caution

Close the container tightly after use in order to prevent contamination with dust or moisture. Avoid direct exposure to sunlight. Store at room temperature.

When Discarding Actuator and Servo Driver



- Please discard as industrial waste.
- Please discard as industrial waste when discarding.

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